

IMPACT BEHAVIOURS OF BIO-INSPIRED SANDWICH BEAM UNDER CONTINUOUS IMPACTS

Tan Juin Hwee

Bachelor of Engineering with Honors (Civil Engineering) 2020

UNIVERSITI MALAYSIA SARAWAK

	Grade:	-
	Please tick (🗸)	
	Final Year Project Report	✓
	Masters	
	PhD	
DECLARATION	N OF ORIGINAL WORK	
This declaration is made on the 10 th AUGU	<u>JST 2020.</u>	
Student's Declaration:		
I, <u>TAN JUIN HWEE from FACULTY</u> entitled, <u>IMPACT BEHAVIOURS</u> <u>UNDER CONTINUOUS IMPACTS</u> sources except where due reference or acl any part been written for me by another p	<u>OF ENGIEERING</u> hereby declare that OF BIO-INSPIRED SANDWICH is my original work. I have not copied from knowledgement is made explicitly in the te erson.	t the work <u>H BEAM</u> n any other ext, nor has
10th ALICLIST 2020	TH.	
<u>10- AUGUST 2020</u>		_
Date submitted	TAN JUIN HWEE (58070)	

Supervisor's Declaration:

I, ASSOCIATE PROFESSOR DR AHMAD KUEH BENG HONG hereby certifies that the work entitled, IMPACT BEHAVIOURS OF BIO-INSPIRED SANDWICH BEAM UNDER CONTINUOUS IMPACTS was prepared by the above named student, and was submitted to the "FACULTY" as a partial KNS 4254 Final Year Project fulfilment for the conferment of BACHELOR OF ENGINEERING WITH HONOURS (CIVIL ENGINEERING), and the aforementioned work, to the best of my knowledge, is the best student's work.

Received for examination by:

(ASSOCIATE PROFESSOR DR AHMAD KUEH BENG HONG)

Date: 10th AUGUST 2020

I declare this Project /Thesis is classified as (Please tick (\checkmark)):

CONFIDENTIAL (Contains confidential information under the Official Secret Act 1972)*

RESTRICTED (Contains restricted information as specified by the organisation where research was done) *

 \square OPEN ACCESS

Student's signature:

Validation of Project/Thesis

I therefore duly affirmed with free consent and willingness declared that this said Project/Thesis shall be placed officially in the Centre for Academic Information Services with the abide interest and rights as follows:

- This Project/Thesis is the sole legal property of Universiti Malaysia Sarawak (UNIMAS).
- The Centre for Academic Information Services has the lawful right to make copies for the purpose of academic and research only and not for other purpose.
- The Centre for Academic Information Services has the lawful right to digitise the content to for the Local Content Database.
- The Centre for Academic Information Services has the lawful right to make copies of the Project/Thesis for academic exchange between Higher Learning Institute.
- No dispute or any claim shall arise from the student itself neither third party on this Project/Thesis once it becomes sole property of UNIMAS.
- This Project/Thesis or any material, data and information related to it shall not be distributed, published or disclosed to any party by the student except with UNIMAS permission.

(10th AUGUST 2020)

Supervisor's signature:

(10th AUGUST 2020)

Current Address: <u>DEPT. OF CIVIL ENGINEERING, FACULTY OF ENGINEERING, 94300 KOTA SAMARAHAN,</u> <u>SARAWAK</u>

Notes: * If the Report is **CONFIDENTIAL** or **RESTRICTED**, please attach together as annexure a letter from the organisation with the period and reasons of confidentiality and restriction.

The following Final Year Project Report:

Title : Impact Behaviours of Bio-Inspired Sandwich Beam under Continuous Impacts

Name : Tan Juin Hwee

Matric No. : 58070

has been read and approved by:

.

(Associate Professor Dr. Ahmad Kueh Beng Hong)

10th August 2020

Date

Project Supervisor

ACKNOWLEDGEMENTS

First and foremost, I would like to express my gratitude to my supervisor, Associate Professor Dr Ahmad Kueh Beng Hong and my co-supervisors, Mr Abd Azim Abdullah and Dr Raudhah Ahmadi for their support, patience and encouragement throughout my graduate studies. They gave me a lot of useful information about the graduate studies. Without the helps from them, I might not be able to complete my graduate studies on time. I felt very grateful to have such excellent and helpful supervisor and co-supervisors like Associate Professor Dr Ahmad Kueh Beng Hong, Mr Abd Azim Abdullah and Dr Raudhah Ahmadi.

Besides that, I would like to thank my beloved family and friends for their support and encouragement throughout my graduate studies.

ABSTRACT

Impact behaviours of newly designed bio-inspired sandwich beam (BHSB) inspired by the woodpecker's head configuration were numerically examined under continuous lowvelocity impact loadings. The newly designed beam contains four main layers, in which carbon fiber reinforced plastic top and bottom skins were employed in sandwiching dualcore consisting of solid hot melt adhesive (HMA) and aluminium honeycomb materials. Innovatively, the solid HMA core was designed in an arch shape. The impact behaviours of the BHSB have been numerically examined by using the finite element software. ABAQUS. Impact loadings were performed in a repeated manner with a hemisphere steel impactor for three impact energy levels of 7.28J, 9.74J, and 12.63J. In all cases, stresses were observed to be mainly concentrated on the impact region while some stresses were distributed to the supports. The new BHSB can resist up to 5 continual impacts at both impact energies of 7.28J and 9.74J but only up to 3 times repeated loads for 12.63J. Besides, impact resistance efficiency index, which assessed the overall impact performance of the sandwich structures, were compared between the newly designed BHSB and the previously designed BHSB. The impact resistance efficiency indices of the newly designed BHSB were found to be 1.31-5.33 times higher, exhibiting an improvement in performance.

ABSTRAK

Tingkah laku impak "bio-inspired sandwich beam" (BHSB) yang baru direka yang diilhami oleh konfigurasi kepala pelatuk kayu diperiksa secara berangka di bawah beban hentaman berkelajuan rendah berterusan. Rasuk yang baru direka mengandungi empat lapisan utama, di mana kulit atas dan bawah "carbon fiber reinforced plastic" digunakan dalam sandwic dual-core yang terdiri daripada "solid hot melt adhesive" (HMA) dan "aluminium honeycomb". Secara inovatif, teras HMA padat direka bentuk dalam bentuk lengkungan. Tingkah laku impak BHSB telah diperiksa secara berangka dengan menggunakan ABAQUS. Beban hentaman dilakukan secara berulang dengan pemukul keluli hemisfera untuk tiga tahap tenaga hentaman 7.28J, 9.74J, dan 12.63J. Dalam semua kes, tekanan diperhatikan terutama tertumpu pada kawasan hentaman sementara beberapa tekanan disalurkan ke sokongan. BHSB baru direka dapat menahan hingga 5 hentaman berterusan pada kedua-dua tenaga hentaman 7.28J dan 9.74J tetapi hanya 3 kali beban berulang untuk 12.63J. Selain itu, indeks kecekapan ketahanan hentaman, yang menilai keseluruhan prestasi hentaman struktur sandwic, dibandingkan antara BHSB yang baru direka dan BHSB yang direka sebelumnya. Indeks kecekapan ketahanan hentaman BHSB yang baru dirancang didapati 1.31-5.33 kali lebih tinggi, menunjukkan peningkatan prestasi.

TABLE OF CONTENTS

Acknowledgementi
Abstractii
Abstrakiii
Table of Contents iv
List of Figures vii
List of Tablesxiii
List of Symbols xiv
CHAPTER 1: INTRODUCTION 1
1.1 Introduction1
1.2 Problem statement
1.3 Aim and objectives
1.4 Scope of study
1.5 Significance of study
CHAPTER 2: LITERATURE REVIEW
2.1 Introduction
2.2 Mechanical behaviour of sandwich structures
2.3 Impact on composite sandwich structure with different geometry 8
2.4 Impact on composite sandwich structure with multi core
2.5 Impact on composite sandwich structure with different impact
energies
2.6 Repeated impact on composite sandwich structure
2.7 Bio-inspired sandwich beam development
2.8 Arch structure
2.9 Literature review remarks

CHAPTER	3: METHODOLOGY	32
	3.1 Introduction	32
	3.2 Bio-inspired sandwich beam development	32
	3.3 Materials and fabrication	33
	3.4 Finite element modelling	35
	3.5 Leg angle of the hyoid layer	36
	3.6 Model construction	38
	3.6.1 CFRP skins	38
	3.6.2 Honeycomb core	. 41
	3.6.3 Arch layer (Hyoid)	. 44
	3.6.4 Impactor	. 47
	3.6.5 Surface assignation	. 52
	3.6.6 Properties and section manager	. 53
	3.6.7 Assembly of model	. 60
	3.6.8 Step module	. 63
	3.6.9 Interaction	. 67
	3.6.10 Boundary condition and impact velocity	. 70
	3.6.11 Meshing	. 74
	3.6.12 Run the model analysis	. 78
	3.6.13 Repeated impact on sandwich structure	, 79
	3.7 Convergence study	. 81
	3.8 Expected findings	83
CHAPTER 4	: RESULT AND DISCUSSION	84
	4.1 Introduction	84
	4.2 Impact behaviour	84
	4.3 Stress propagation	87
	4.4 Sandwich beam failure modes	92

	4.5 Displacement, velocity and acceleration of impactor	
	4.6 Absorbed energy	100
	4.6 Impact resistance efficiency index calculation	104
CHAPTER S	5: CONCLUSION	109
	5.1 Conclusion	109
	5.2 Recommendations	
REFERENC	ES	111

••

•

٠

LIST OF FIGURES

Figure

Figure 1.1. Failure modes of sandwich beams: (a) loading configuration, (b) face yielding,
(c) face wrinkling, (d) core yielding and (e) indentation2
Figure 1.2. Sections of cross-ply GFPP-reinforced aluminium foam sandwich structures
subjected to impact energies between 13 J and 73 J
Figure 2.1. Out-of-plane compressive behaviour: (a) stress vs. strain curve and (b) the
compressive failure modes
Figure 2.2. Shear behaviour of the pyramidal truss core sandwich structure: (a) stress vs.
strain curve and (b) the shear failure modes
Figure 2.3. Energy absorption per unit volume of the sandwich structures by varying the
thicknesses
Figure 2.4. Predicted damage areas for various core densities
Figure 2.5. Variation of (a) percentage of absorbed energy with respect to impact energy,
and (b) peak load against core densities 10
Figure 2.6. Damage evolution in sandwich structures with different core thickness 11
Figure 2.7. The variation of the maximum impact force with impact mass for a constant
impact energy of 0.97J 12
Figure 2.8. The variation of the maximum impact force with impact energy for two 13mm
thick aluminium honeycomb beams
Figure 2.9. Energy partition graph showing how the incident energy is absorbed by
sandwich structures based on 13 mm thick core
Figure 2.10. The influence of beam length on the impact response of the thicker sandwich
structures14
Figure 2.11. The influence of beam length on the impact response of the thicker sandwich
structures14
Figure 2.12. Energy partition curves showing the way of incident energy is absorbed by
sandwich structures based on a 25 mm thick core
Figure 2.13. Low velocity impact simulation on type C sandwich structure with 9 m/s
(60J): deformation plots, internal energy and force curves

Figure 2.14. Low velocity impact simulation on type D sandwich structure with 9 m/s
(60J): deformation plots, internal energy and force curves 17
Figure 2.15. High velocity impact simulation on type C sandwich structure with 64 m/s
(27J): deformation plots, kinetic energy curve of impactor and cross-section
Figure 2.16. High velocity impact simulation on type D sandwich structure with 132 m/s
(117J): deformation plots, kinetic energy curve of impactor and cross-section
Figure 2.17. Contact force-deflection histories for samples with one-core, two-core and
three-core impacted at: (a) 10J, (b) 20J, (c) 35J and (d) 50J19
Figure 2.18. The energy profile diagrams of one-core, two-core and three-core samples
Figure 2.19. Fibre-failure criterion contour plot at different stages during simulation: (a)
impact energy 15 J and (b) impact energy 35 J 20
Figure 2.20. Evolution of the equivalent plastic strain (PEEQ) on the core during the
simulation: Impact energy 15 J 21
Figure 2.21. Evolution of the equivalent plastic strain (PEEQ) on the core during the
simulation: Impact energy 35 J 21
Figure 2.22. Comparison between the percentage of energy absorbed and the percentage
of dissipated plastic energy vs. impact energy. Numerical results
Figure 2.23. Force-time histories for the 25 mm impactor at (a) 1 J and (b) 15 J 23
Figure 2.24. Comparison of experimental and numerical (a) maximum displacement and
(b) peak force results as a function of impact energy
Figure 2.25. Initially constructed failure mode maps for applied energy of 13.5 J at (a)
2nd impact; (b) 3rd impact; (c) 4th impact; (d) 5th impact
Figure 2.26. Modified failure mode maps for repeated impacted at (a) 13.5 J; (b) 15.55 J;
(c) 21.43 J
Figure 2.27. Head configuration of woodpecker
Figure 2.28. Mechanical vibration analysis of a woodpecker (beak, hyoid, skull bone and
brain) under drumming impact without considering the spongy bone. (a) Dynamic
response. (b) Frequency spectrum diagram of the dynamic response of a brain. The
relatively high frequency vibrations of the brain during $t = 0$ to 2 ms, which can cause g-
force-induced loss of consciousness or brain damage to the woodpecker, indicate that the
spongy bone eliminates the initial high-frequency vibrations as a mechanical low-pass
filter
Figure 2.29. Bio-inspired honeycomb sandwich beam

Figure 2.30. Injury profiles by category	30
Figure 3.1. The idealized model for the bio-inspired sandwich beam	33
Figure 3.2. Stress strain plot for solid hot melt adhesive (HMA) specimens	34
Figure 3.3. Flowchart in modelling the sandwich structure by using ABAQUS	36
Figure 3.4. Geometric structure for hyoid layer.	37
Figure 3.5. Parabolic curve for the hyoid layer.	37
Figure 3.6. Core configuration of bio-inspired honeycomb sandwich beam with	solid
HMA layer in arch shape with 36° angle.	38
Figure 3.7. "Create part" sketcher toolbox.	39
Figure 3.8. Sketcher viewport	39
Figure 3.9. Step of creating partition for top part of CFRP skin.	40
Figure 3.10. Create partition viewport	40
Figure 3.11. Copying CFRP-T for CFRP-B.	41
Figure 3.12. "Create construction: line at an angle" button is pressed	42
Figure 3.13. Single honeycomb core's cell.	42
Figure 3.14. Translate a single honeycomb core's cell.	43
Figure 3.15. Arrangement of honeycomb core cell.	43
Figure 3.16. Honeycomb core with dimension of 300 mm x 25 mm x 20 mm	44
Figure 3.17. Rectangular cross-section of hyoid.	44
Figure 3.18. Rectangular hollow section of the hyoid	45
Figure 3.19. Step to extrude the rectangular hollow section.	45
Figure 3.20. Arc lines drawn on the selected surface.	46
Figure 3.21. Arc lines are trimmed on the selected surface	46
Figure 3.22. Completed extruded arch layer.	47
Figure 3.23. A circle and two lines are drawn for the hemisphere shape	47
Figure 3.24. Drawn quadrant.	48
Figure 3.25. Completed hemisphere shape	48
Figure 3.26. Drawn circle with 6 mm radius.	49
Figure 3.27. Completed cylinder.	49
Figure 3.28. Separated parts of cylinder and hemisphere	50
Figure 3.29. Rotating the cylinder.	50
Figure 3.30. Clicking on "merge/cut instance".	51
Figure 3.31. Merging impactor from cylinder and hemisphere	51
Figure 3.32. "Create surface" dialog box.	52

Figure 3.33. Selecting the whole CFRP-B for surface assignation.	52
Figure 3.34. (a) Bottom surface of CFRP-B; (b) Top surface of CFRP-B	53
Figure 3.35. Material behaviour of HMA	55
Figure 3.36. Material behaviour of aluminium honeycomb core	56
Figure 3.37. Material behaviour of (a) CFRP skin; (b) Impactor.	56
Figure 3.38. "Edit inertia" dialog box for the impactor	57
Figure 3.39. "Edit section" dialog box for hyoid	58
Figure 3.40. "Section manager" dialog box	58
Figure 3.41. Stacking sequence of CFRP skins (Abo Sabah et al., 2018)	59
Figure 3.42. "Edit section" dialog box for (a) CFRP-T; (b) CFRP-B	59
Figure 3.43. "Edit section" dialog box for (a) aluminium honeycomb core; (b) in	npactor.
	59
Figure 3.44. Section assignment for the hyoid.	60
Figure 3.45. Assembly the CFRP-T and impactor.	61
Figure 3.46. Final model of bio-inspired sandwich beam.	62
Figure 3.47. Spacing in between part instances	62
Figure 3.48. "Edit step" dialog box.	63
Figure 3.49. Field output 1.	65
Figure 3.50. "Edit history output request" for (a) H-Output-2; (b) H-Output 3	66
Figure 3.51. "Edit history output request" for (a) H-Output-4; (b) H-Output 5	66
Figure 3.52. "Edit history output request" for H-Output-6	67
Figure 3.53. Impactor and upper part of top layer CFRP skin are selected to refine	contact
domain	68
Figure 3.54. Creating interaction property.	68
Figure 3.55. Contact property for (a) Tangential behaviour; (b) Normal behaviou	ır 69
Figure 3.56. Example of viewport in constraint manager.	70
Figure 3.57. "Create boundary condition" dialog box	70
Figure 3.58. Boundary conditions for (a) core side; (b) CFRP-T edges; (c) CFRF	P-B; (d)
hyoid sides; (e) impactor	73
Figure 3.59. Value of impactor velocity is inserted in the predefined field	74
Figure 3.60. Prescribing predefined velocity for the impactor	74
Figure 3.61. "Global seeds" dialog box for CFRP-T.	75
Figure 3.62. Seed edges for middle and both end region of CFRP-T	75
Figure 3.63. Seed edges for in between of middle and both end region of CFRP-7	Г 76

Figure 3.64. Completed mesh of CFRP-T	76
Figure 3.65. Element size for hyoid	77
Figure 3.66. "Element type" dialog box for the hyoid layer	77
Figure 3.67. Creating and editing the job	78
Figure 3.68. Viewport of visualization module	79
Figure 3.69. Steps to carry out the second impact	79
Figure 3.70. Model attributes for second impact is edited	30
Figure 3.71. Example of viewport of predefined field in the load module for secon	ıd
impact	31
Figure 3.72. Displacement against 1/element size for hyoid layer	32
Figure 4.1. Contact force against time for energy level of 7.28 J	35
Figure 4.2. Contact force against time for energy level of 9.74 J	36
Figure 4.3. Contact force against time for energy level of 12.63 J	36
Figure 4.4. Maximum stresses at the bottom skins of sandwich beam for 7.28 J 8	37
Figure 4.5. Maximum stresses at the bottom skins of sandwich beam for 9.74 J 8	8
Figure 4.6. Maximum stresses at the bottom skins of sandwich beam for 12.63 J 8	8
Figure 4.7. Skin stress distribution for first impact at impact energy level of 7.28 J (a	a)
CFRP-B (b) hyoid 8	9
Figure 4.8. Skin stress distribution for first impact at impact energy level of 9.74 J (a	a)
CFRP-B (b) hyoid	0
Figure 4.9. Skin stress distribution for first impact at impact energy level of 12.63 J (a	a)
CFRP-B (b) hyoid9	1
Figure 4.10. FEM simulation for (a) BHSB at Ei=7.28 J (5th impact); (b) BHSB at	at
Ei=9.74 J (5th impact); (c) BHSB at Ei=12.63 J (3rd impact)	3
Figure 4.11. FEM simulation at the end of impactor loading after the impactor bounce	2S
back to its original location for (a) BHSB at Ei=7.28 J (5th impact); (b) BHSB at Ei=9.7	4
J (5th impact); (c) BHSB at Ei=12.63 J (3rd impact)	4
Figure 4.12. FEM mid-section deformed shape for (a) BHSB at Ei=7.28 J (5th impact));
(b) BHSB at Ei=9.74 J (5th impact); (c) BHSB at Ei=12.63 J (3rd impact)	4
Figure 4.13. Graph of displacement of impactor against time for Ei = 7.28 J, 9.74 J and	d
12.63 J	6
Figure 4.14. Graph of velocity of impactor against time for Ei = 7.28 J, 9.74 J and 12.63J	J.
	7

Figure 4.15. Graph of acceleration of impactor against time for $Ei = 7.28$ J,	9.74 J and
12.63 J	99
Figure 4.16. Energy-time curves for Ei = 7.28 J, 9.74 J and 12.63 J	102
Figure 4.17. Absorbed energy for Ei = 7.28 J, 9.74 J and 12.63 J	103
Figure 4.18. Bar chart on impact resistance efficiency index against number	of impacts
for each impact energy level	108

•

.

.

LIST OF TABLES

Table

.

Page

Table 3.1. Mechanical properties of solid HMA	34
Table 3.2. Aluminium honeycomb core cell material properties	34
Table 3.3. EP-1006 adhesive properties	35
Table 3.4. Properties of the unidirectional T350/EP-1006 composite	35
Table 3.5. Conversion of stress and strain values	55
Table 3.6. Convergence study for hyoid layer	82
Table 3.7. Element number for each layer of sandwich structure	82
Table 4.1. Impact resistance efficiency index for HSB, BHSB and BHSB with hyoid la in arch shape	iyer 106
Table 4.2. Impact resistance efficiency index for BHSB with hyoid layer in arch sh for impact energy level of 7.28 J.	ape 107
Table 4.3. Impact resistance efficiency index for BHSB with hyoid layer in arch sh for impact energy level of 9.74 J.	ape 107
Table 4.4. Impact resistance efficiency index for BHSB with hyoid layer in arch sh for impact energy level of 12.63 J	ape 107

.

LIST OF SYMBOLS

σ_{f}	- Global longitudinal strength of skin material
σ_c	- Core compressive strength
τ _c	- Core shear strength
l _e	- Impact resistance efficiency index
E _{abs}	- Absorbed energy
F _{max}	- Maximum contact force
A _d	- Damage area
g	- Gravitational acceleration
m _b	- Mass of sandwich beam
t	- Thickness of sandwich beam
σ_{max}	- Maximum stress in sandwich beam

.

.

CHAPTER 1

INTRODUCTION

1.1 Introduction

Chai and Zhu (2011) defined that composite sandwich panel is made up of two stiff and thin skins with a lightweight, thick and low modulus core. This composite sandwich structure has a high value of the strength/weight ratio. It is not only relatively lightweight however it can support transverse loads more efficiently. Usage of sandwich structures are commonly found in many engineering application such as marine and transport industries, aerospace and aircraft industries.

According to Chai and Zhu (2011), it has been widely examined the impact loads exerted on the composite sandwich panels by using of experimental techniques, mathematical modelling and also numerical methods. As composite sandwich structures are widely applied in engineering application and they are prone to failure due to impact load, there are some areas of research are still interesting being pursued such as contact analysis between the impactor and the composite surfaces, the response of structure after impact, the failure mechanism by impact, the residual property after impact, high-velocity impact analysis and impact analysis of soft body impactor.

Abo Sabah et al. (2019) stated some failure models of sandwich beams during the lowvelocity impact test such as face wrinkle, face yield, indentation and core failure. According to Abrate (1998), core buckling, delamination in the impacted face sheet, core cracking, matrix cracking and fibre breakage in the facings have been identified as the failure modes of sandwich beams. In general, beam's geometry and properties of the materials for skin layer and core layer can affect the type of failures. Damages are usually existed on the top layer of structure only as low-velocity impact does not lead to

1

perforation to the structure whereas minor damage and core shearing are involved in the bottom layer of structure. Face yielding is meant by the surface of structure that undergoes fracture completely due to micro-tension. Besides that, face wrinkling is meant by the skin that undergoes some matrix cracking and fibre breakage as micro-compression without the occurrence of fracture.





Figure 1.2 shows that failure of glass fibre reinforced polypropylene (GFPP) sandwich structures with 10 mm thick closed cell aluminium foam block subjected to impact energies. From the figure 1.2, it can be clearly found that it is very dangerous when continuous impact energies exerted on the sandwich structures. If such failure occurs on the structure built, human safety will being threatened for more severe consequences.



Figure 1.2. Sections of cross-ply GFPP-reinforced aluminium foam sandwich structures

subjected to impact energies between 13 J and 73 J (Villanueva & Cantwell, 2004).

1.2 Problem statement

Concept of sandwich construction still remains interesting though composite sandwich structures have been used for non-strength part of structures in the last decade. Due to complexity nature of sandwich structures, the investigation of impact behaviour of composite sandwich beam under different continuous impact energies remains an active research topic. Different impact load conditions can bring a direct risk to the life span of the sandwich structures. More serious consequences can be expected in structurally and also in terms of human safety. The consequences can be more severe if the loading environment is in the presence of impact and blasting.

Past researches had shown that several factors which are stiffness, damping and mass of structure can influenced the impact response of a sandwich structure. A good sandwich structure is not only higher in value of the strength/weight ratio but it should be higher resistance to extreme continuous load magnitude.

From the research works done before, it can be clearly seen that composite sandwich structures are vulnerable to impact-induced damages. Impact behaviour and impact efficiency of sandwich beam with core layer in arch shape is an interesting topic and still not being studied. Impact resistance of sandwich structure is very important to ensure that the structure can last longer and sustain more loadings exerted on it. The inspiration of using core layer in arch shape comes from the cultural of Roman development which they believed arch structures can sustain more loads on it.

Hence, current research work is conducted to investigate the impact behaviour of sandwich beam with the solid hot melt adhesive (HMA) layer in arch shape due to varying continuous impact energies. The main purpose of forming an arch shape for solid HMA layer is inspired by the woodpecker's hyoid structure so that impacted load can be mitigated effectively. Solid HMA layer with an arch shape can transfer the compressive load to the support at two ends effectively because the force exerted are tangential to the end of arch.

1.3 Aim and objectives

The main objectives of the research work are:

- i. To develop a composite sandwich beam finite element model under impact loading.
- ii. Numerically examine the impact behaviour of the sandwich beam due to varying impact energies.
- iii. Compute the impact efficiency of the sandwich beam due to different impact energies.

4

1.4 Scope of study

- i. The sandwich beam is a C-clamp supported at two ends.
- ii. There are two cores and one skin material used for the sandwich beam.
- iii. The skin material is made of carbon fibre reinforced plastic (CFRP) whereas core materials are made of solid hot melt adhesive (HMA) as core I and aluminium honeycomb as core II.
- iv. Three levels of continuous impact energy: 7.28J, 9.74J and 12.63J are applied perpendicularly to centre of the sandwich beam.
- v. Dimension of the sandwich beam is 300 mm long, 25 mm wide and 25.4 mm thick.
- vi. The stacking sequence of skin is $[0/\mp 30]$.
- vii. The model of bio-inspired aluminium honeycomb sandwich beam has the solid HMA core layer in arch shape with angle of 36°.
- viii. The finite element software, ABAQUS/CAE 6.13-1, is used for the impact modelling.

1.5 Significance of study

As usage of composite sandwich structures can be commonly found in many engineering application, extensive works have been carried out numerically. It is very complex and having unique behaviour in resisting the impact loading. Hence, the impact behaviour of composite sandwich structure under continuous impact loading was examined in order to improve their performance under services condition.

Solid HMA as the core I of the composite sandwich structure was designed in arch shape with 36° of arch leg which can absorb impact energy efficiently and transfer it to the support safely without damaging the skin layer of the sandwich beam.

CHAPTER 2

LITERATURE REVIEW

2.1 Introduction

This chapter generally discussed on the previous research works on the composite sandwich structure. Important points such as problems considered, method used and main result of previous research work are extracted in details in this chapter.

2.2 Mechanical behaviour of sandwich structures

Mechanical test was carried out by Wang et al. (2010) as only few investigations on the mechanical properties of sandwich structures with carbon fiber-reinforced pyramidal lattice truss core have been carried out. Wang et al. (2010) carried out the compression and shear tests by using the Instron 5569 universal testing machine at the room temperature and displacement rate of 0.5 mm min⁻¹ which followed the standards from ASTM C365 and C273.

Four samples are tested in the compressive test. The representative compressive stressstrain is shown in Figure 2.1a. Based on the stress-strain curve, initial linear response is occurred followed by the peak compressive stress. This point is occurred when the failure of the truss member is first to be observed. After that, value of stresses decreases subsequently when strain is increasing with the serrations in the compressive stress vs strain curves. Based on Figure 2.1b, failure mode of the sandwich structures were observed during the compressive test which are splitting and buckling of the truss members.